PATENT SPECIFICATION

(11) **1424698**

80 (9 (9) (9)

(21) Application No. 17076/73

(22) Filed 10 April 1973

(31) Convention Application No. TE 645

(32) Filed 20 April 1972 in

(33) Hungary (HU)

(44) Complete Specification published 11 Feb. 1976

(51) INT CL² D06M 15/72

(52) Index at acceptance

B2E 184 186 187 18Y 199 204 20Y 23Y 246 299 302 329 339 361 44Y 463 46Y 478 483 498 548 580 588 603 60X 60Y 620 634 637 63Y 65Y 673 67Y 683 695 696 708 720 72X 758 768 798

D1P A1 B2A2 B2B1 B2BX B5B C2A10 C2A12A1 C2A12A4 C2A12A5 C2A12AX C2A12B2 C2A12BX C2A2B C2A2C C2A8 C2C2 C2C3 C2C7 C2C8 C2C9 C2CX



(54) PRODUCTION OF AN IMPROVED FINISH IN TEXTILE PRODUCTS

(71) We, INTERCOOPERATION KERESKEDELEMFEJLESZTÉSI RT., of 14, Attila ut, Budapest I, Hungary, a body corporate organized under the laws of Hungary, do hereby declare the invention for which we pray that a patent may be granted to us, and the method by which it is to be performed, to be particularly described in and by the following statement:—

The invention concerns a process for the production of a finish of layered structure and heterogeneous distribution developed on filaments of cellulosic fibrous materials, yarns or woven or knitted fabrics, or for example cellulosic textile products mixed with synthetic filament materials, with the aid of which the dry and wet crease recovery and the dimensional stability of the listed products may be significantly increased, and their abrasion resistance or tearing strength may be considerably improved, relative to known finishes of similar intended use.

It is known that the dry and wet recovery of textile products of cellulose based singlecomponent filamentary materials, or of such materials mixed with synthetic filamentary materials, is limited. In order to improve the crease recovery, one proceeds by cross-linking the cellulose itself or by applying a crosslinkable material to the celluose. It is characteristic of such finishing treatments that the tendency for resilient shape recovery of celulose-based products is improved, but the tearing strength and abrasion resistance considerably deteriorate.

The technical aim sought to be attained, i.e. the improvement of crease recovery and dimensional stability without appreciable deterioration of abrasion resistance and tearing strength could in principle be achieved with a heterogeneous finish which is capable of simultaneously satisfying these partially mutually contradictory requirements. As witnessed by the technical literature, recently

numerous proposals have been made with which the desired aims may be achieved only partially but not to a sufficient extent or only by employing very expensive means; in other words experiments performed to develop layers of heterogeneous structure have not so far assured the desired result.

In effect, the reduction of abrasion resistance may be attributed to the condensed or cross-linked synthetic resin layer applied to the outer surface of the filament, the formation of which layer is required from the point of view of dimensional stability and crease recovery in the textile material. However, no known proposal has been successful in obviating the attendant deterioration in abrasion resistance and tearing strength, and consequently requirements regarding crease recovery, resilience and dimensional stability have been met only at the expense of wear resistance and tearing strength of textile products.

Several research workers have been engaged in transforming the surface layer of textile products to be treated. A. W. Reeves (Amer. Dyestuff Rep. 57, 37—41 /1968/) sought to solve the transformation of surface layer by applying polymers to the surface of the fabric.

Authors Gogek and Valkó (Textilveredlung 2, 423—428 /1967/) performed numerous experiments to produce a cross-linking agent of heterogeneous distribution to be formed in the textile product and unambiguously ascertained that this could not be achieved in an aqueous medium. For removing the water-soluble, cross-linkable monomer applied to the filament surface they employed a mixture of water and ethyl alcohol or water and acetone. Another of their proposed solutions is that they wished to prevent cross-linking by an anti-catalyst slowly diffusing into the filament, or by de-

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activating the acidic catalysts by an alkaline solution in aqueous alcohol.

A. E. Lauchenauer and his collaborators (Text. Res. J. 39, 585-603 /1969/) deactivated the catalyst on the filament surface with ammonia. According to the experiments of authors Meier and Zollinger (Textilveredlung 5, 709—720 / 1970 /) the catalyst in the outer layer of the filament may be disabled 10 by triethylene tetramine in a polar solvent. Author J. Willard and his collaborators (Text. Res. J. 39, 413-421 /1969/) developed a process for directional cross-linking achievable in the core of the cotton fila-15 ment by solubilizing the cross-linking monomer before condensation from the outer layer of the filament by means of an organic solvent.

None of the listed methods has found 20 significant or widespread use in industry.

The aim of the present invention is the production, by relatively simple technological means, of a synthetic resin finish on cellulosic filament textile products which is of heterogeneous distribution by a process which, on the one hand, ensures optimum crease recovery and dimensional stability of the treated products, and on the other hand, reduces to the minimum possible magnitude 30 the inevitable reduction in tearing strength and abrasion resistance, relative to the starting material, which accompanies the production of the finish.

According to the invention there is provided a process for producing a layered finish on the fibres of cellulosic textile fabrics wherein the fabrics or fibres from which they are to be made are saturated with a watersoluble cross-linkable synthetic resin monomer and/or cligomer and a cross-linking catalyst so that some of the monomer and/or oligomer and catalyst diffuse into the fibres; the monomer and/or oligomer and catalyst are washed from the surface of the fibres by 45 means of an aqueous sol of a colloidal surface-active substance which forms a resilient film on the fibres without diffusing into them; and the monomer and/or oligomer diffused into the fibres and the said substance are fixed to the fibres by crosslinking of the monomer and/or oligomer and dry-

Preferably, a further layer is applied to the uppermost layer of the colloidal material by 55 treating the latter, before fixing, with an aqueous solution of compounds suitable for making a covalent bond with the colloidal material and of the general formula (I)-(VI), as shown in the accompanying drawing, wherein R is CH_2 — $(CH_2)_n$ and n=10—

As monomer and/or oligomer we prefer to employ dimethylol-methylene carbamide, dimethylol - dihydroxy - ethylene - car-65 bamide, trimethylol - melamine, hydroxy -

ethyl - thiazone, hexamethylol - melamine, dimethylol - carbamide or similar monomers or oligomers. The cross-linking catalyst may be selected from the following group of $MgCl_2$, $ZnCl_2$, $(NH_1)_2SO_4$, compounds: $Al_2(SO_4)_2$, $Zn(NO_3)_2$, ammonium tartrate and substances of similar effect.

As surface-active film-forming, colloidal materials we prefer to employ protein derivatives cross-linked to colloidal form with aldehydes, carboxymethyl - cellulose, cellulose ethers or starch ethers, partially polyvinyl alcohol, acetylated methylol melamine-based acid colloid, aqueous polyurethane dispersions or other similar materials. As representative compounds suitable for developing covalent bonds for cellulose we mention N - stearyl - acrylamide, stearyl - methyl - pyridine - ether, N stearyl - methylamide - methylene -pyridine chloride.

The colloidal material may be employed in an aqueous preparation which also contains the cross-linkable monomer and/or oligomer, a cross-linking catalyst, expediently in a concentration which amounts to a minimum of 50% and a maximum of 200% by weight of the concentration used in the first seturating solution.

We have found it advantageous that the impregnation with the cross-linkable synthetic resin monomer and/or oligomer and the catalyst should be performed with a padder or with other machine treatment of equivalent effect. We proceed similarly for the treatment with the surface active material, and in given cases also with the production of the further layer applied to the textile product.

A characteristic of the process according 105 to the invention is that no drying or condensation is required between the individual operations performed with different materials, in spite of which the desired technical aim can be achieved to a greater extent than hitherto. The material to be treated may be e.g. a cotton or bast fibre fabric, hemp, China grass or mixtures of these with regenerated cellulose, a fabric of cotton mixed with polyester, regenerated cellulose-based or linen 115 fabric.

The invention is based on the discovery that with the described process discrete layers of heterogeneous distribution may be formed in the cross-section of the filamentary material to be treated. To this end the simplest solution would appear to be provison of directional cross-linking by rinsing with an aqueous solution (on the basis of osmotic pressure) the washing effect of which 125 is limited exclusively to the surface of the filaments. Since the diffusion of the crosslinking monomer during penetration and during drying is of opposite effect to the rinsing, washing or rinsing, experiments per- 130

formed with water have not been successful. Attempts have been made, in known manner, to eliminate the difficulties arising from the extremely rapid forward and back diffusion of the monomer, by reducing the swelling of the filament, washing with organic solvents, or using surface catalyst poisons.

We see it as important that we perform the removal of the cross-linking material from 10 the surface layer of the textile product with an aqueous solution with apparatus of limited washing effect. A padder is suitable for this purpose. Performing the removal step of the cross-linking material once or twice, a hetero-15 geneous filament structure may be developed which remains even after the succeeding dry-

ing and condensation steps.

Thus, in practising the invention, first the cross-linkable, water-soluble, synthetic resin 20 monomer, and/or the oligomer formed therefrom, and the catalyst are applied by impregnation to the filament or fabric to be treated. Thereafter, suitably without intermediate drying, the cross-linkable, water-25 soluble component and the catalyst are expelled from the surface of the treated materials by a washing with an aqueous sol of surface-active colloidal material which is water-soluble or dispersible in water, does 30 not diffuse into the material, it is desired to treat, and is resilient and film-forming. The place of the component removed from the filament surface is occupied by the material of colloidal state and size and after the 35 succeeding drying and condensation steps the two components form a heterogeneous, sandwich-type micromolecular system.

With the process according to the invention the abrasion resistance of the surface layer may be improved by applying further resiliency - improving and plasticising materials. One proceeds as follows: after applying the colloidal material to the material to be treated but without inter-45 posing a drying step, the uppermost layer of colloidal material applied to the surface is washed off, as by padding with a solution of a surface-active softening substance which is capable of forming a covalent bond with the colloidal material, and thus the colloidal material disposed on the surface is displaced. To apply this further layer compounds specified in the above description are

employed.

After application of these various materials the treated product is dried at a temperature of 70-100°C to a moisture content of 5-15%, and condensation is effected in 2-6 minutes at a temperature between 13-160°C. While a following rinsing and drying of the textile material is recommended, this may be deferred until the first aqueous treatment (washing) of the textile material.

The general result of the process accord-65 ing to the invention is that the dry and wet crease recovery and dimensional stability of cellulose-based filaments or textile products are significantly improved while the abrasion resistance of the filament is good.

The process according to the invention is further described by the following non-limit-

ing Examples.

Example 1

Cotton fabric was saturated with a solution of 100-150 g/litre 50% dimethylol ethylene - carbamide and 10—15 g/litre MgCl₂ at a temperature between 20-30°C and a pressure efficiency of 85% by a padder at a rate of 30 m/min. Then, without intermediate drying, the treated cotton fabric was padded with a gelatine solution, pretreated with formaldehyde, at 40°C and at the previous rate.

After the padding treatment the treated cotton fabric is dried on a tentering frame at a temperature around 100°C, and condensed

for 5 minutes at 140°C.

Example 2

Cotton fabric was saturated with a solution of 100-120 g/litre 50% hexamethylolmelamine and 3—5 g/litre NH₄(SO₄)₂ at a temperature between 20—30°C using a 85% pressure efficiency on a padder at a rate of 30 m/min. Then, without intermediate drying, the treated cotton fabric was treated in a padder by a 40°C polyvinyl alcohol solution pretreated with 3-5 g/litre formaldehyde.

The treated fabric was subjected to further processing in the manner according to Ex-

ample 1.

Example 3

A mixed fabric of 67% cotton and 33% polyester was padded by a solution of 100-150 g/litre, 50% dimethylol - ethylene carbamide and 10—15 g/litre magnesium chloride at a temperature between 20-30°C and 85% pressure efficiency. Without intermediate drying a padding treatment was carried out at 40°C with a solution of 1-8 g/litre polyvinyl alcohol pretreated with formaldehyde and 6-24 g/litre magnesium chloride.

The treated fabric was subjected to further processing in the manner according to Example 1.

Example 4

A regenerated cellulose-based fabric was treated in a padding apparatus with a solution of 100-150 g/litre, 50% dimethylol ethylene - carbamide and 10-15 g/litre 120 MgCl₂ at a temperature between 20-30°C, at a rate of 50 m/min. and 85% pressure efficiency. Then, without intermediate drying, the treated fabric was padded with a solution of 20-100 g/litre acid colloid, pre- 125

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pared as described below, at a temperature between 20-40°C.

To prepare the acid colloid solution, 300 g 50% trimethylol melamine was mixed with 30 g 85%, phosphoric acid, then the mixture was diluted with 600 ml water and heated in a mixer at 50°C for approximately one hour; after adding 50 g trimethylamine the reaction mixture was allowed to cool to room 10 temperature to obatin a colloidal condensate.

The two layers applied to the regenerated cellulose-based fabric treated as described above were subjected to finishing processes (drying and condensation) according to

15 Example 1.

Example 5

A linen fabric was treated according to Example 3, with the difference that after the second padding treatment, without intermediate drying, the treated fabric was further treated with a solution of 50—103 g/litre concentration of N-stearyl acrylamide cr a solution of stearyl - methylamidomethylene - pyridine chloride of similar con-centration. The final drying and condensing process were carried out according to Example 1.

The improved properties of textile products treated according to the invention are summarised in the following Table:

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TABLE

	Method of Preparation	Abrasion cycle no. (n)* Stoll	Weight loss (Accelerator)	Crease reco	overy angle o wet
35	Mercerised and bleached fabric without synthetic resin Mercerised and bleached fabric,	3250	6.8	67	73
40	treated with synthetic resin in the known manner Mercerised and bleached fabric,	757	39.5	114	123
	treated by process according to the invention	1451	24.1	117	126

* flexed and abraded in a Stoll QM Abrasion testing machine abrasion with Accelerator, three minutes at 3000 r.p.m.; area of abraded surface 136× 136 mm.

WHAT WE CLAIM IS:-

1. A process for producing a layered finish on the fibres of cellulosic textile fabrics wherein the fabrics or fibres from which they are to be made are saturated with a watersoluble cross-linkable synthetic resin monomer and/or oligomer and a cross-linking catalyst so that some of the monomer and/or oligomer and catalyst diffuse into the fibres; 55 the monomer and/or oligomer and catalyst are washed from the surface of the fibres by means of an aqueous sol of a colloidal surface-active substance which forms a resilient film on the fibres without diffusing into 60 them; and the monomer and/or oligomer diffused into the fibres and the said substance are fixed to the fibres by cross-linking of the monomer and/or oligomer and dry-

2. A process as claimed in claim 1 wherein a further layer is applied to the uppermost layer of the colloidal material by treating the latter, before fixing, with an aqueous solution of compounds suitable for making a 70 covalent bond with the colloidal material and of the general formula (I)—(VI), where R is CH_1 — $(CH_2)_n$ and n=10-16.

3. A process as claimed in claim 1 or 2 wherein as monomer dimethylol - ethylene

75 carbamide, dimethylol - dihydroxy ethylene - carbamide, trimethylol - melamine,

hydroxy - ethyl - thiazone, hexamethylol melamine, dimethylol - carbamide, or similar monomer, is employed.

4. A process as claimed in any preceding claim wherein as catalyst one or more of the following compounds are employed: MgCl₂, ZnCl₂, (NH₄)₂SO₄, Al₂(SO₄)₂, Zn(NO₃)₂.

5. A process as claimed in any preceding claim wherein as surface-active, film-forming, colloidal materials protein derivatives crosslinked to colloidal form with aldehydes, carboxyl - methyl - cellulose, cellulose ethers or starch ethers, partially acetylated polyvinyl alcohol, methylol melamine-based acid colloid, or aqueous polyurethane dispersions, are used.

6. A process as claimed in claim 2 or any appendant thereto, wherein the material suitable for forming covalent bonds with the filamentary material is chosen from N - stearyl - acrylamide, stearyl - methyl pyridine - ether or N - stearyl - methylamide - methylene - pyridine - chloride.

7. A process as claimed in any preceding 100 claim wherein a colloidal aqueous preparation of the surface active substance is employed which, in addition to the cross-linkable synthetic resin monomer and/or oligomer, also contains a cross-linking catalyst, in a 105 concentration which amounts to a minimum of 50% and a maximum of 200% by weight

of the concentration used in the first saturating solution.

8. A process as claimed in any preceding claim wherein the treatment (impregnation) with the cross-linkable synthetic resin monomer and/or oligomer and catalyst is carried out by padding.

9. A process as claimed in any preceding claim wherein the treatment with the surfaceactive material is carried out by padding.

10. A process according to claim 2 or any claim appendant thereto, wherein the further layer is applied to the material to be treated by padding.

11. A process as claimed in any preceding claim wherein consecutive layer-applying steps are carried out without intermediate drying and condensation.

12. A process as claimed in any preceding claim wherein the material to be treated is any one of cotton fabric, a mixed fabric of

cotton and polyester, regenerated cellulosebased fabric or linen fabric.

13. A process as claimed in any of claims 8 to 12 wherein the padding is carried out at a rate of 30—150 m/min.

14. A process as claimed in claim 1 substantially as herein described with reference to the Example.

15. A textile product having a finish produced by a process as claimed in any preceding claim.

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Printed for Her Majesty's Stationery Office, by the Courier Press, Learnington Spa, 1976.
Published by The Patent Office, 25 Southampton Buildings, London, WC2A 1AY, from which copies may be obtained.

1 SHEET

This drawing is a reproduction of the Original on a reduced scale

(1),

(II),

$$R-N=C=0$$

(VI)